

Integrated silicon nitride electro-optic modulators with atomic layer deposited overlays

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Silicon nitride (SiN) is currently the most prominent CMOS-compatible platform for photonics at wavelengths <1 μm . However, realizing fast electro-optic (EO) modulators, the key components of any integrated optics platform, remains challenging in SiN. Modulators based on the plasma dispersion effect, as in silicon, are not available. Despite the fact that significant second-harmonic generation has been reported for silicon-rich SiN, no efficient Pockels effect-based modulators have been demonstrated. Here we report the back-end CMOS-compatible atomic layer deposition (ALD) of conventional second-order nonlinear crystals, zinc oxide, and zinc sulfide, on existing SiN waveguide circuits. Using these ALD overlays, we demonstrate EO modulation in ring resonators. © 2019 Optical Society of America

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Today, silicon photonics is unmistakably one of the main photonic integration platforms. A key contributor to its success is the use of CMOS infrastructure for fabrication of photonic chips, enabling low-cost photonic integrated circuits (PICs), along with the possibility of electronic-photonic co-integration. Next to the established silicon-on-insulator (SOI) platform, plasma-enhanced chemical vapor deposition (PECVD) silicon nitride (SiN) is gaining ground as a back-end CMOS-compatible material platform. Unlike silicon, SiN is transparent in the visible wavelength range [1]. Together with its low losses, it opens roads to new applications.

Electro-optic (EO) modulators are very useful components to have on a photonics platform. With the ever increasing demand for data, cheap, efficient, and fast optical modulators are in high demand. Next to telecom and datacom, other application areas are emerging where integrated SiN phase modulators can play an important role: programmable PICs for, e.g., microwave photonics and quantum information processing [2,3], and optical phased arrays for, e.g., LIDAR and holographic 3D displays, requiring visible wavelength operation [4].

On the SOI platform, the plasma dispersion effect is exploited to realize fast EO modulators [5]. SiN however, is an insulating

material, making the free charge carrier-based approach non-viable. Another well-known approach to EO modulation is the use of the Pockels effect. Lithium niobate (LiNbO_3) is particularly known for its large Pockels effect. Moreover, it is transparent in the visible and near-infrared wavelength range. Low-voltage integrated LiNbO_3 modulators operating at 1550 nm have been demonstrated [6]. However, the use of thin film LiNbO_3 -on-insulator requires expensive bonding procedures. Unfortunately, the second-order nonlinearity of SiN and, consequently the Pockels effect, is expected to vanish due to SiN's amorphous nature. Yet, EO modulation has been demonstrated in low-loss LPCVD (low pressure CVD) SiN, albeit with small EO coefficients of maximum 8.31 ± 5.6 fm/V at 1550 nm [7]. In addition, second-harmonic generation has been observed in SiN films [8] and waveguides [9]. Experiments indicate the existence of a bulk nonlinearity which appears to be strongest in silicon-rich SiN films. It is yet unclear whether large Pockels coefficients in low-loss waveguides can be achieved.

As SiN itself offers no clear-cut solutions for optical modulation, apart from the slow and inefficient thermo-optic effect [10], there have been attempts to combine SiN with other materials. Combining graphene with SiN, Phare *et al.* demonstrated a high-speed electro-absorption modulator at 1550 nm [11]. The fabrication was done by transferring CVD graphene on copper to a planarized SiN PIC. Mehta *et al.* showed efficient modulation in SiN-on- LiNbO_3 Mach-Zehnder modulators at 674 nm [12]. Only DC characterization was performed. The modulators were fabricated by depositing PECVD SiN on a LiNbO_3 substrate. Lead zirconate titanate (PZT) thin films have been used to demonstrate high-speed PZT-on-SiN modulators in the O- and C-band, with the possibility of extension to visible wavelengths [13]. However, the PZT deposition involves annealing at a temperature of 620°C, which can cause Cu diffusion in the underlying CMOS electronics for back-end deposited photonic circuits [14]. In addition, AlN has been proposed as an alternative CMOS-compatible platform which is transparent at wavelengths <1 μm and allows for EO modulation [15].

In this Letter, we demonstrate monolithically integrated SiN-based fast EO ring modulators operating at 0.9 μm , a wavelength

often used in LIDAR systems [16]. The modulators are realized by overlaying SiN waveguides with atomic layer deposited (ALD) EO materials, namely zinc oxide (ZnO) or zinc sulfide (ZnS). ALD is a low-temperature conformal deposition technique compatible with CMOS fabrication technology [17]. Our approach does not require poling. Poled materials can suffer from long-term stability issues, especially at elevated operating temperatures. ZnO is a wide bandgap material (≈ 3.4 eV) that crystallizes preferably in the hexagonal wurtzite structure, point group 6 mm [18]. 6 mm is a non-centrosymmetric point group, allowing for a Pockels effect. For bulk ZnO crystals, Pockels coefficients of $|r_{33}| = 2.6$ pm/V and $|r_{13}| = 1.4$ pm/V are reported at a wavelength of 0.63 μm [19]. ZnS exists in two main non-centrosymmetric crystalline phases: the hexagonal wurtzite structure (bandgap ≈ 3.9 eV) and the cubic zinc-blende structure, point group $\bar{4}3m$ (bandgap ≈ 3.7 eV) [20]. At a wavelength of 0.63 μm , Pockels coefficients of $|r_{33}| = 1.9$ pm/V and $|r_{13}| = 0.9$ pm/V are reported for the wurtzite phase [19], and $|r_{41}| = 1.9$ pm/V for the zinc-blende phase [21]. To the best of our knowledge, no Pockels coefficients have been reported for these materials in thin films.

Our SiN waveguides are patterned in a CMOS pilot line using 193 nm deep UV lithography. The SiN layer has a thickness of 300 nm and is deposited by LPCVD on top of a 3.3 μm SiO₂ layer. On the patterned waveguides, the ALD materials are deposited (thicknesses in a 70 – 100 nm range) in a homebuilt setup with a base pressure of 10^{-6} mbar. A standard ALD cycle consists of a 5 s exposure for the precursor/co-reactants and a 25 s purge time between each exposure. The pressure of the precursor/co-reactants is set to 5×10^{-3} mbar, unless stated otherwise. For the ZnO layers, two processes were used, both at a substrate temperature of 300°C : a plasma-enhanced ALD (PE-ALD) process using diethylzinc (DEZ) and 10 s oxygen plasma exposures (10^{-2} mbar), and a plasma-enhanced thermal ALD (PET-ALD) process using the exposure sequence DEZ–H₂O– 10 s O₂ plasma. The O₂ plasma is generated by a radio frequency inductively coupled generator, operated at 13.56 MHz and 200 W power. ZnS layers were deposited by a thermal process (TH-ALD) using DEZ and H₂S at a substrate temperature of

150°C . In addition, the use of a 6 nm Al₂O₃ seed layer (deposited prior to the ZnO/ZnS layer) was investigated, as it has been shown to promote ZnO crystallite growth where the *c*-axis is perpendicular to the substrate [22,23]. This leads to an enhanced second-order nonlinearity. Al₂O₃ was deposited using trimethylaluminum and H₂O at a substrate temperature of 120°C . After ALD, a layer of bisbenzocyclobutene (BCB) is spin coated and cured to serve as waveguide cladding. Figure 1(a) shows an SEM image of a waveguide cross section. Next, Ti/Au (Ti improves adhesion) electrodes are patterned in a ground-signal-ground (GSG) configuration utilizing a lift-off process. Figure 1(b) shows a fabricated device. Finally, the chips are cleaved to allow for edge coupling.

X-ray diffraction (XRD) θ - 2θ scans were performed to check the crystallinity of our ALD thin films (Fig. 2). For ZnO, the 002 reflection is clearly observed for all the tested ALD recipes, indicating that the crystallites preferentially grow with their *c*-axis normal to the substrate [22]. For the PET-ALD ZnO, we can see that adding a thin Al₂O₃ layer increases the 002 reflection. For ZnS, there are peaks at 28.2° and 32.7° . The former can be ascribed to the 111 reflection of cubic ZnS [24], and the latter can be ascribed to the forbidden 200 reflection of the silicon substrate whose amplitude depends on the in-plane sample rotation [25]. The addition of Al₂O₃ slightly enhances the crystallinity. We expect textured films to be beneficial in preserving as much as possible of the single-crystal material nonlinearity.

Since our polycrystalline ALD films possess in-plane isotropy (∞m symmetry), the non-zero elements of their Pockels tensor are $r_{13} = r_{23}$, $r_{51} = r_{42}$, and r_{33} , with 3 referring to the normal to the film plane [15]. By choosing the electrode configuration illustrated in Fig. 1(c), we get an out-of-plane electric field in the film on the waveguide top surface, so we can probe r_{13} (for TE modes) and r_{33} (for TM modes). The effective index change of the guided mode depends on the EO coefficients, the overlap of the optical mode with the EO active layer, and the electric field induced by the electrodes [26]. In choosing the BCB cladding thickness, there is a trade-off between minimal absorption loss by the metal and maximum electric field in the thin film. We have BCB thicknesses of ≈ 1.6 μm (measured from the top of the SiO₂ layer) for the ZnO-based devices and ≈ 1.5 μm for the ZnS-based devices. This gives an estimated (from mode simulations) absorption loss on the order of 0.001 dB/cm for the fundamental quasi-TE mode and 0.01 dB/cm for the quasi-TM mode, for a SiN waveguide width of 800 nm at a wavelength of 0.9 μm . The signal electrode width is chosen to be 2 μm wider than the waveguide width to have some tolerance against misalignment in the

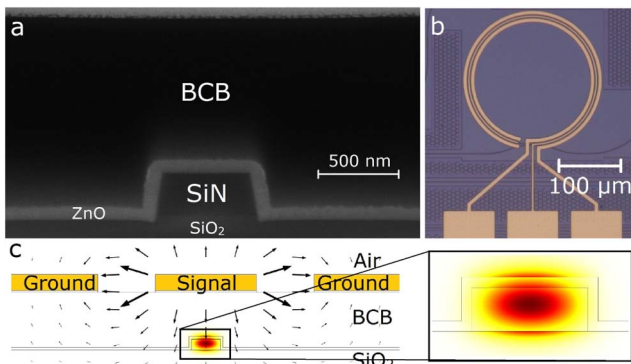


Fig. 1. (a) SEM image of the cross section of a SiN waveguide with 6 nm Al₂O₃, 81 nm PET-ALD ZnO, and a BCB cladding. (b) Microscope image of a fabricated modulator. Rectangular contact pads are used for landing a GSG probe. (c) Schematic cross section of a ZnO-covered SiN waveguide with electrodes. The intensity of the fundamental quasi-TM optical mode is shown, along with the electric field induced by the electrodes (arrows). 13% of the mode power resides in the ALD overlay.

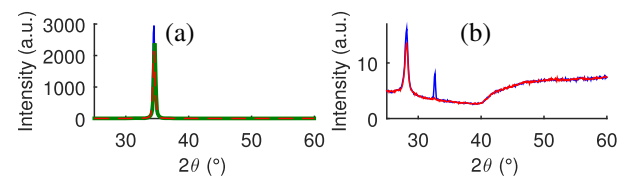


Fig. 2. XRD θ - 2θ scans using Cu $K\alpha$ radiation for (a) 81 nm PET-ALD ZnO with 6 nm Al₂O₃ seed layer (blue), 81 nm PET-ALD ZnO (red), 62 nm PE-ALD ZnO (green), and (b) 30 nm TH-ALD ZnS with 6 nm Al₂O₃ seed layer (blue), 27 nm TH-ALD ZnS (red). All films are deposited on silicon substrates with native oxide (thickness on the order of 1 nm).

Table 1. Propagation Loss for a SiN Waveguide Width of 800 nm, for the Fundamental Quasi-TE and -TM Mode

ALD Overlay	α_{TE} (dB/cm)	α_{TM} (dB/cm)
No ALD overlay	1.1 ± 0.5	0.9 ± 0.2
PE-ALD ZnO	11 ± 4	12 ± 2
PET-ALD ZnO	4 ± 2	3.9 ± 0.6
PET-ALD ZnO + Al ₂ O ₃	4.6 ± 0.7	6 ± 2
TH-ALD ZnS	4 ± 1	9 ± 2
TH-ALD ZnS + Al ₂ O ₃	3.0 ± 0.8	7.9 ± 0.8

lithography process. The gap between the signal and ground electrodes is 1.6 μm . This gap size is limited by the resolution of our contact mask. Smaller gaps would result in larger electric fields, but can give issues during lift-off. In addition, smaller gaps increase the probability of dielectric breakdown. To convert the effective index change induced by the EO effect into a change in optical power, we use 100 μm radius ring resonators. The coupling gaps between the ring and bus waveguides vary from 200 to 450 nm (excluding the ALD layer).

Both transmission and modulation measurements were conducted on the fabricated devices. In the transmission measurements, light from a tunable laser is coupled in and out of the chip via lensed fibers. The polarization is controlled with a fiber polarization controller. The resonances in the transmission spectrum can be fitted, which gives us the self-coupling coefficient r and single-pass amplitude transmission a . Since various coupling gaps are available, r and a can be distinguished from one another, thus allowing us to get an estimate of the propagation loss [27]. Table 1 summarizes the estimated propagation losses for a SiN waveguide width of 800 nm at a wavelength of 0.9 μm . Figure 3(a) shows an example of a transmission measurement.

For the modulation measurements we apply a small AC voltage $U(t) = U_{\text{peak}} \sin(2\pi ft)$ with a GSG probe. The transmitted light is led to a photodetector of which the RF output is connected to an electrical spectrum analyzer (ESA). On the ESA, a peak is observed at the same frequency as the applied voltage. From the ESA peak height, the variation in optical power ΔP_{out} can be calculated ($P_{\text{out}}(t) = P_{\text{out},0} + \Delta P_{\text{out}} \sin(2\pi ft)$). Figure 3(a) shows how ΔP_{out} changes when the laser wavelength is tuned (for a fixed U_{peak} and f). We see the maximum on the slopes of the res-

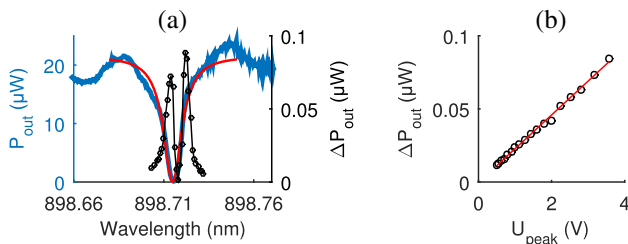


Fig. 3. Transmission and modulation measurements performed on a SiN with ZnS overlay (thickness of 100 nm) ring modulator with a gap of 350 nm and a waveguide width of 800 nm for the quasi-TE mode. (a) Blue, transmitted optical power measured as a function of wavelength; red, fitting of resonance; black, modulation amplitude of transmitted optical power ΔP_{out} measured as a function of the wavelength for $f = 10$ MHz and $U_{\text{peak}} = 3.6$ V. (b) Black circles, measurement of ΔP_{out} as a function of U_{peak} for $f = 10$ MHz and a wavelength of 898.721 nm. Red line, linear fitting of data.

onance, while ΔP_{out} drops significantly at the bottom of the resonance and when tuning away from resonance. A slight shift in resonance occurred during the measurements. Figure 3(b) illustrates the linear variation of ΔP_{out} with the applied voltage U_{peak} . The aforementioned observations concur with a linear EO effect. The same behavior was seen for all the tested modulators. From the slope of the fitted line in Fig. 3(b) and the first-order derivative of the transmission spectrum at the bias point, the $V_{\pi}L$ product can be estimated:

$$V_{\pi}L \approx \frac{\lambda^2 L}{n_{\text{eff}}^4 4\pi R} \frac{\frac{\partial P_{\text{out}}}{\partial \lambda}}{U_{\text{peak}}}, \quad (1)$$

with λ being the wavelength, L being the electrode length, n_{eff} being the effective refractive index of the optical mode, and R being the ring radius. For the ZnO-based devices, we got the following $V_{\pi}L$ estimates for the quasi-TE (TM) mode: 6(4) V \cdot m for PE-ALD, $1 \times 10(2 \times 10)$ V \cdot m for PET-ALD, and 6(5) V \cdot m for PET-ALD with Al₂O₃. For the ZnS-based devices, we found for the quasi-TE (TM) mode 2 $\times 10(3 \times 10)$ V \cdot m without Al₂O₃ and 3 $\times 10(2 \times 10)$ V \cdot m with Al₂O₃. For SiN modulators without an ALD overlay, we estimated $1 \times 10^2(2 \times 10^2)$ V \cdot m for the quasi-TE (TM) mode. For the PET-ALD ZnO overlay, the addition of Al₂O₃ improves $V_{\pi}L$, which can be related to the improved crystallinity. For the ZnS overlay, no significant improvement was observed. The PE-ALD ZnO overlay gives $V_{\pi}L$ values similar to the PET-ALD ZnO with Al₂O₃ overlay, but the loss is larger for the PE-ALD ZnO overlay.

In addition, the EO response was measured for increasing modulation frequency (Fig. 4). As the Pockels effect is an ultrafast effect, the bandwidth is expected to be limited by the cavity photon lifetime τ and/or the resistance-capacitance time constant. The 3 dB bandwidth can be estimated from $1/f_{3\text{dB}}^2 = 1/f_Q^2 + 1/f_{RC}^2 = (2\pi\tau)^2 + (\pi(50\Omega + 2R)C)^2$, where 50 Ω is the output impedance of the signal generator and termination of the probe; R and C are the series resistance and capacitance of the device [5]. From S_{11} parameter measurements, we found $C = 140$ fF and $R = 200\Omega$. For the ZnS-based modulators and blank SiN modulator measured in Fig. 4(b), we estimated the photon lifetimes τ and corresponding $f_{3\text{dB}}$: 29 ps, corresponding to 3.7 GHz (red), 37 ps, corresponding to 3.3 GHz (blue), and 97 ps, corresponding to 1.5 GHz (black). The observed bandwidths are somewhat smaller; however, this is not unusual, as the above-mentioned empirical formula does not account for coupling conditions and wavelength [5]. For the ZnO-based modulators, none of the above explains the ≈ 100 MHz

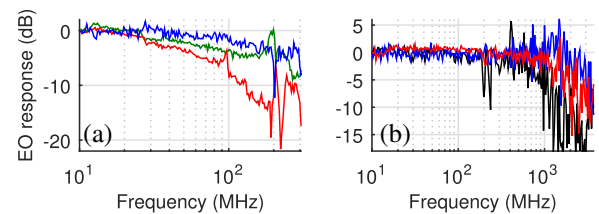


Fig. 4. EO response of modulators versus modulation frequency. (a) PE-ALD ZnO (green), PET-ALD ZnO (red), and PET-ALD ZnO with Al₂O₃ (blue). (b) TH-ALD ZnS (red), TH-ALD ZnS with Al₂O₃ (blue), and SiN without ALD overlay (black).

bandwidths. ZnO is known to possess n-type conductivity due to the presence of defects and impurities [28]. The free charge carriers could play a role in the modulation mechanism. The resistivity ρ of the ALD films was measured with a four-point probe. For the PE-ALD ZnO films, we found $\rho \approx 10 \Omega \cdot \text{cm}$. For all other ZnO and ZnS films, ρ was above the measurement limit ($>10^4 \Omega \cdot \text{cm}$). The PET-ALD recipe was used specifically to increase ρ and decrease the carrier concentration [29]. Although ρ was increased by several orders of magnitude, this had no significant influence on the bandwidth. To investigate the role of free carriers in the modulation mechanism and extend the bandwidth, a more in-depth material exploration is required, including annealing treatments and depositions at different temperatures to alter the film's resistivity [28].

From the knowledge of $V_{\pi}L$, the simulated electrostatic and optical field distributions, the Pockels coefficients can be estimated [26]. For SiN, we estimate $|r_{33}| \approx 0.01 \text{ pm/V}$ and $|r_{13}| \approx 0.02 \text{ pm/V}$. For ZnS (with Al_2O_3), we find $|r_{33}| \approx 0.3 \text{ pm/V}$ (0.4 pm/V) and $|r_{13}| \approx 0.2 \text{ pm/V}$ (0.1 pm/V). These values are smaller than those reported for bulk ZnS crystals, as expected for polycrystalline films. For PE-ALD ZnO, we estimate $|r_{33}| \approx 3 \text{ pm/V}$ and $|r_{13}| \approx 2 \text{ pm/V}$. For PET-ALD ZnO (with Al_2O_3), we find $|r_{33}| \approx 0.5 \text{ pm/V}$ (2 pm/V) and $|r_{13}| \approx 0.7 \text{ pm/V}$ (2 pm/V). Some of these values are larger than those reported for bulk ZnO crystals, which also hints to the fact that other mechanisms play a role in the refractive index modulation.

Although the estimated $V_{\pi}L$ values are large, we do not need a full π phase shift in our ring resonators to realize switching or modulation with a large extinction ratio. For instance, for a critically coupled ring with a loss of 5 dB/cm, switching between the minimum transmission (0 at critical coupling) and a transmission of -3 dB (not including coupling and access waveguide loss) requires only 2% of V_{π} .

By adapting the waveguide dimensions and electrode configuration, further improvements in $V_{\pi}L$ can be made. First, the modal overlap with the EO ALD layer can be increased by reducing the SiN thickness and/or increasing the ALD layer thickness. Secondly, the electric field strength can be increased by lowering the ground electrodes (placing them in trenches etched in the SiO_2 next to the waveguide). This can reduce the $V_{\pi}L$ product by at least a factor of 5. Other measures to increase the field strength are the use of transparent conducting oxides as electrodes which can be placed very close to the waveguide core [30], or using of nanoplasmonic SiN slot waveguides [31].

In conclusion, we demonstrated fast SiN-based EO ring modulators by overlaying SiN PICs with an EO material, namely ZnO or ZnS. These materials are deposited by ALD, a low-temperature deposition technique compatible with CMOS fabrication technology. Considering the lack of CMOS-compatible SiN-based EO modulators, our results are very valuable.

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